

Intrinsic Rotation Generation as a Plasma Flow Engine Process

Y. Kosuga, P.H. Diamond, Ö.D. Gürçan and J.E. Rice

CASS and CMTFO, UCSD, USA
WCI Center for Fusion Theory, NFRI, RoK
CNRS, France
PSFC, MIT, USA

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Motivation

“We must attribute to heat the great movements that we observe all about us on the Earth. Heat is the cause of currents in the atmosphere, of the rising motion of clouds, of the falling of rain and of other atmospheric phenomena ...”

S. Carnot, 1824 → alumnus of Ecole Polytechnique

⇒ Role of **heat** in driving fluid motions

⇒ Is there a simple physics concept underlying **intrinsic rotation** in tokamaks?

⇒ How and Why does intrinsic rotation scale with plasma parameters?



Outline

- ▶ Background \Rightarrow A paradigm: Intrinsic Rotation as **Heat Engine**
- ▶ **Entropy**: setting-up “engine” calculation
 - ▶ relation to δf^2 balance \rightarrow production and nonlinear coupling
 - ▶ Stationary state with $\langle V_E' \rangle \rightarrow$ akin to improved confinement
- ▶ Plasma Flow **Engine**
 - ▶ Intrinsic Rotation (IR) as a consequence of engine process
 \rightarrow Conversion of Heat (∇T) to Flow ($\langle V_{\parallel} \rangle$) by **residual stress**
 - ▶ Comparison to experiment, C-Mod data:

$$\frac{\langle V_{\parallel} \rangle}{v_{thi}} \cong \frac{\rho_*}{2} \frac{\chi_i}{\chi_{\phi}} \sqrt{\frac{T_i}{T_e}} \frac{L_s}{L_T} \sim 0.18$$

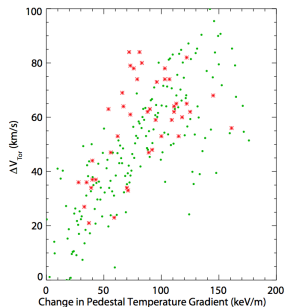
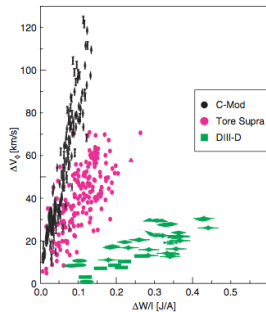
- ▶ Conclusion

Background

- ▶ Tokamak plasmas observed to rotate via input of heat, in the absence of obvious momentum input → **Intrinsic Rotation**
- ▶ Scalings in **improved** confinement:

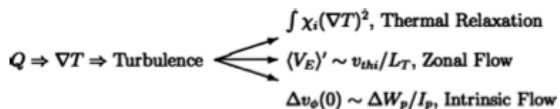
	H-mode	I-mode
Global	$\Delta v_\phi \sim \Delta W_p / I_p$	$\Delta v_\phi \sim \Delta W_p / I_p$
Local	$\Delta v_\phi \sim \nabla p \sim \nabla T$	$\Delta v_\phi \sim \nabla T$

⇒ $\Delta v_\phi \sim \nabla T$ **both** in H- and I-mode



Background, Engine

- ▶ a la Carnot and $\Delta v_\phi \sim \nabla T \rightarrow$ a consequence of “engine” process



Y.K. et al '10

- ▶ How **quantify** plasma as engine?
 - ▶ **Entropy** budget of plasma \rightarrow evolution via heat input, flow generation, spatial flux of entropy, ...
 - ▶ Based on the entropy budget, modeling of $\Pi_{r||}^{res}(\nabla T, V_E', \dots)$

Entropy (Coarse grained) $\Rightarrow \langle \delta f^2 \rangle$ evolution

- ▶ Entropy evolution: $\partial_t \int d\Gamma \langle \delta f^2 \rangle / \langle f \rangle \sim \partial_t S_0$, $S_0 \equiv - \int d\Gamma \langle f \rangle \ln \langle f \rangle$: Entropy from coarse grained f , $d\Gamma \equiv d^3v d^3x$
- ▶ $\langle \delta f^2 \rangle \rightarrow$ Drift kinetic equation for ions + adiabatic electrons

$$\partial_t f + v_{\parallel} \nabla_{\parallel} f + \frac{c}{B} \hat{\mathbf{z}} \times \nabla \tilde{\phi} \cdot \nabla f + \frac{|e|}{m_i} \tilde{E}_{\parallel} \frac{\partial f}{\partial v_{\parallel}} = C(f), \quad \frac{\delta n_e}{n_0} = \frac{|e| \tilde{\phi}}{T_e}$$

- ▶ Entropy/ $\langle \delta f^2 \rangle$ evolution:

$$\int d\Gamma \left\{ \frac{\partial \langle \delta f^2 \rangle}{\partial t} \frac{1}{2 \langle f \rangle} + \frac{\partial \langle \tilde{V}_x \delta f^2 \rangle}{\partial x} \frac{1}{2 \langle f \rangle} + \nu_c \frac{\langle \delta f^2 \rangle}{\langle f \rangle} \right\} = \underbrace{\int d^3x \mathcal{P}}_{\text{production rate}}$$

where $C(\delta f) = -\nu_c \delta f$

- ▶ RHS: **Production rate** \mathcal{P}

$$\mathcal{P} \equiv \int d^3v \left\{ -\langle \tilde{V}_r \delta f \rangle \frac{\langle f \rangle'}{\langle f \rangle} - \frac{e}{m} \frac{\langle \tilde{E}_{\parallel} \delta f \rangle}{\langle f \rangle} \frac{\partial \langle f \rangle}{\partial v_{\parallel}} \right\}$$

\rightarrow free energy in configuration and velocity space

- ▶ LHS: **spatial transport** of $\langle \delta f^2 \rangle$ /entropy + Collisional dissipation

RHS: Production rate

$$\int d^3x \mathcal{P} = \int d\Gamma \left\{ -\langle \tilde{V}_r \delta f \rangle \frac{\langle f \rangle'}{\langle f \rangle} - \frac{e}{m} \frac{\langle \tilde{E}_{\parallel} \delta f \rangle}{\langle f \rangle} \frac{\partial \langle f \rangle}{\partial v_{\parallel}} \right\}$$

$$= \int d^3x \left\{ \underbrace{-\frac{n \langle T_i \rangle'}{T_i^2} \langle \tilde{V}_r \tilde{T} \rangle - \frac{n \langle V_{\perp} \rangle'}{v_{thi}^2} \langle \tilde{V}_r \tilde{V}_{\perp} \rangle - \frac{n \langle V_{\parallel} \rangle'}{v_{thi}^2} \langle \tilde{V}_r \tilde{V}_{\parallel} \rangle}_{\text{spatial part, } \langle \dots \rangle' \text{ and } \langle \tilde{V}_r \delta f \rangle \rightarrow \text{Heat flux, mom. flux } \perp \& \parallel} + \frac{1}{T_i} \langle \tilde{J}_{\parallel}^i \tilde{E}_{\parallel} \rangle \right\}$$

Parallel heating

- ▶ Spatial Part: Generic form of **entropy production**, $\sum_i \mathcal{J}_i \mathcal{X}_i$ where

Generalized Fluxes: $\mathcal{J}_i = \{ \langle \tilde{V}_r \tilde{T} \rangle, \langle \tilde{V}_r \tilde{V}_{\perp} \rangle, \langle \tilde{V}_r \tilde{V}_{\parallel} \rangle \}$

Thermodynamic Forces: $\mathcal{X}_i = \{ -\langle T \rangle', -\langle V_{\perp} \rangle', -\langle V_{\parallel} \rangle' \}$

→ Need modeling of $\mathcal{J}_i[\mathcal{X}_i]$, **Flux-Gradient relation**

- ▶ Velocity part: Parallel heating

Production, $O(k_{\perp})$

$$\int d^3x \mathcal{P} = \int d^3x \left\{ \boxed{-\frac{n\langle T \rangle'}{T_i^2} \langle \tilde{V}_r \tilde{T} \rangle} - \boxed{\frac{n\langle V_{\perp} \rangle'}{v_{thi}^2} \langle \tilde{V}_r \tilde{V}_{\perp} \rangle} - \frac{n\langle V_{\parallel} \rangle'}{v_{thi}^2} \langle \tilde{V}_r \tilde{V}_{\parallel} \rangle + \frac{1}{T_i} \langle \tilde{J}_{\parallel} \tilde{E}_{\parallel} \rangle \right\}$$

→ dominant terms, $O(k_{\perp})$: Heat input, Zonal Flow growth

▶ $\langle \tilde{V}_r \tilde{T} \rangle = -\chi_i \langle T \rangle'$, χ_i turbulent thermal conductivity

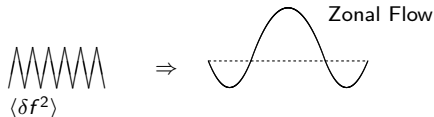
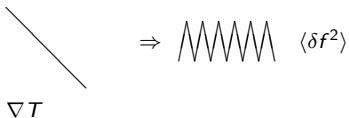
▶ **positive definite**: $\chi_i \langle T \rangle'^2 > 0$
→ **production** of $\langle \delta f^2 \rangle$ /entropy

▶ $\langle \tilde{V}_r \tilde{V}_{\theta} \rangle \rightarrow$ wave kinetic equation

$$\langle \tilde{V}_r \tilde{V}_{\theta} \rangle = K \langle V_E' \rangle, \quad K \equiv \sum_k \frac{k_{\theta}^2 \rho_s^2 c_s^2}{\Delta \omega_k} \left(-k_r \frac{\partial \langle \eta_k \rangle}{\partial k_r} \right)$$

$$\langle \eta_k \rangle = (1 + k_{\perp}^2 \rho_s^2)^2 |\hat{\phi}_k|^2, \quad K = \gamma_{ZF} L_i^2$$

▶ **negative definite**: $-K \langle V_E' \rangle^2 < 0$ when $\gamma_{ZF} > 0$
→ **destruction** of $\langle \delta f^2 \rangle$ /entropy



Production, spatial, Mom. Flux (\parallel)

$$\int d^3x \mathcal{P} = \int d^3x \left\{ \frac{n\chi_{turb}^i}{L_T^2} - \frac{nK\langle V'_E \rangle^2}{v_{thi}^2} - \frac{n\langle V_{\parallel} \rangle'}{v_{thi}^2} \langle \tilde{V}_r \tilde{V}_{\parallel} \rangle + \frac{1}{T_i} \langle \tilde{J}_{\parallel}^i \tilde{E}_{\parallel} \rangle \right\}$$

- Mean field model: $\langle \tilde{V}_r \tilde{V}_{\parallel} \rangle = -\chi_{\phi} \langle V_{\parallel} \rangle' + \Pi_{r\parallel}^{res}$ \rightarrow neglect pinch for simplicity

- At a stationary state $\langle \tilde{V}_r \tilde{V}_{\parallel} \rangle = 0$; however, it consists of **non-trivial competing parts**

► Diffusive part

\rightarrow turbulent viscous heating

► **positive definite**: $\chi_{\phi} \langle V_{\parallel} \rangle'^2 > 0$

\rightarrow **production** of $\langle \delta f^2 \rangle$

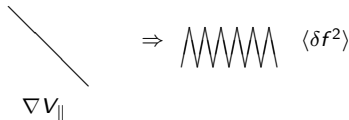
► Work done by **residual stress**

\rightarrow generation of net rotation

► **negative definite**:

$-\langle V_{\parallel} \rangle' \Pi_{r\parallel}^{res} = -(\Pi_{r\parallel}^{res})^2 / \chi_{\phi} < 0$

\rightarrow **destruction** of $\langle \delta f^2 \rangle$



LHS: What competes vs Production?

Entropy/ $\langle \delta f^2 \rangle$ balance:

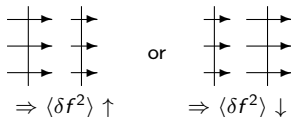
$$\int d\Gamma \left\{ \frac{\partial \langle \delta f^2 \rangle}{\partial t} \frac{1}{2\langle f \rangle} + \frac{\partial \langle \tilde{V}_x \delta f^2 \rangle}{\partial x} \frac{1}{2\langle f \rangle} + \nu_c \frac{\langle \delta f^2 \rangle}{\langle f \rangle} \right\} = \int d^3x \mathcal{P}$$

flux of entropy collision production rate

- ▶ Spatial transport of $\langle \delta f^2 \rangle$
 - ▶ **jump** in the flux through boundaries

$$\int_{x-\Delta}^{x+\Delta} dx \frac{\partial \langle \tilde{V}_x \delta f^2 \rangle}{\partial x} = \left. \frac{\langle \tilde{V}_x \delta f^2 \rangle}{2\langle f \rangle} \right|_{x-\Delta}^{x+\Delta}$$

→ effective local **production** or **destruction** of $\langle \delta f^2 \rangle$



- ▶ Collisional dissipation → local **decrement** of $\langle \delta f^2 \rangle$

$\langle \delta f^2 \rangle$ balance and stationarity

δf^2 balance (with $O(k_\perp)$ production):

$$\int d\Gamma \left\{ \frac{\partial}{\partial t} \frac{\langle \delta f^2 \rangle}{2\langle f \rangle} + \frac{\partial}{\partial x} \frac{\langle \tilde{V}_x \delta f^2 \rangle}{2\langle f \rangle} + \frac{\nu_c \langle \delta f^2 \rangle}{\langle f \rangle} \right\} = \int d^3x \left(\frac{n\chi_i}{L_T^2} - \frac{nK \langle V_E' \rangle^2}{v_{thi}^2} \right)$$

$\Rightarrow \langle V_E' \rangle^2$ at a stationary state,

$$\boxed{\frac{K \langle V_E' \rangle^2}{v_{thi}^2} = \underbrace{\overline{\left(\frac{\chi_i}{L_T^2} \right)}}_{\text{local production}} - \underbrace{\frac{1}{n} \int d^3v \left\{ \frac{\langle \tilde{V}_x \delta f^2 \rangle}{2\langle f \rangle} \Big|_{x-\Delta}^{x+\Delta} \right\}}_{\text{jump in } \delta f^2 \text{ flux}} + \underbrace{\frac{\nu_c \overline{\langle \delta f^2 \rangle}}{\langle f \rangle}}_{\text{local decrement}}}$$

where $\overline{(\dots)} \equiv (2\Delta)^{-1} \int_{x-\Delta}^{x+\Delta} dx(\dots)$

► $\langle V_E' \rangle^2$ set by:

- **heat input** \rightarrow local production of $\langle \delta f^2 \rangle$
- **jump in $\langle \delta f^2 \rangle$ -flux: de/increment** of $\langle \delta f^2 \rangle \rightarrow$ **de/increase** $\langle V_E' \rangle^2$
- local destruction of $\langle \delta f^2 \rangle$ from collision \rightarrow reduce $\langle V_E' \rangle^2$

Residual stress

- ▶ $\langle V'_E \rangle \rightarrow$ residual stress $\Pi_{r\parallel}^{res}(\nabla T_i, \langle V'_E \rangle, \dots) \rightarrow$ intrinsic rotation $\langle V_{\parallel} \rangle$
- ▶ A specific model for $\Pi_{r\parallel}^{res} \rightarrow$ Gurcan et al '07 and Diamond et al '08

- ▶ Net wave momentum

$\rightarrow k_{\parallel}$ symmetry breaking by $\langle V'_E \rangle$ (O.G. et al '07)

$$\left\langle \frac{k_{\parallel}}{k_{\theta}} \right\rangle_{spec} = \frac{\rho_*}{2} \frac{\langle V'_E \rangle}{c_s / L_s}$$

- ▶ Transport of wave momentum

\rightarrow residual stress on flow (P.D. et al '08)

$$\begin{aligned} \Pi_{r\parallel}^{res} &= \sum_k k_{\parallel} v_{g,r} \left\{ -\frac{1}{\Delta\omega_k} \left[v_{g,r} \frac{\partial \langle N_k \rangle}{\partial r} - k_{\theta} \langle V'_E \rangle \frac{\partial \langle N_k \rangle}{\partial k_r} \right] \right\} \\ &\cong \left\langle \frac{k_{\parallel}}{k_{\theta}} \right\rangle_{spec} K \langle V'_E \rangle, \quad K \equiv \sum_k k_{\theta}^2 \Delta\omega_k^{-1} v_{g,r} \frac{\partial \langle N_k \rangle}{\partial k_r} \end{aligned}$$



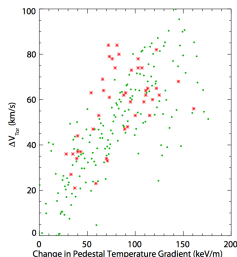
Toroidal Flow

Residual stress, triplet closure + integrating $-\chi_\phi \langle V_{\parallel} \rangle' + \Pi_{r\parallel}^{res} = 0$ yields...

$$\frac{\langle V_{\parallel} \rangle}{v_{thi}} = \frac{\frac{\rho_*}{2} \sqrt{\frac{T_i}{T_e}} \frac{\chi_i}{\chi_\phi} \frac{L_s}{|L_T|}}{\nabla T \text{ driven, } \propto \nabla T / B_\theta} - \frac{\frac{\rho_*}{2} \sqrt{\frac{T_i}{T_e}} \frac{L_s}{2\Delta} \frac{1}{n} \int d^3v \int^{x'} dx' \frac{1}{\chi_\phi} \left(-D_{spr} \frac{\partial}{\partial x} \frac{\langle \delta f^2 \rangle}{2\langle f \rangle} \right) \Big|_{x' - \Delta}^{x' + \Delta}}{\langle \delta f^2 \rangle\text{-flux driven} \rightarrow \text{jump in } \langle \delta f^2 \rangle \text{ flux}}$$

where $D_{spr} = \sum_p Re(g_p) c_s^2 |\hat{\phi}|_p^2$ and $g_p = (-i\omega + ip_{\parallel} v_{\parallel} + ip_{\theta} \langle V_E \rangle + \Delta\omega_p)^{-1}$

- ▶ ∇T driven part $\propto \nabla T / B_\theta$
 - ▶ ∇T scaling both in I- and H-mode
 - ▶ B_θ^{-1} : Inverse current scaling
 - through $L_s \propto q \propto B_\theta^{-1}$
- ▶ $\langle \delta f^2 \rangle$ -flux driven part
 - ▶ $\langle \tilde{V}_x \delta f^2 \rangle \cong -D_{spr} \langle \delta f^2 \rangle'$ after a closure
 - ▶ could be large with **wave-particle resonance**
 - phase space density granulation



$$\Delta v_\phi(0) \sim \nabla T_{edge}$$

An application: Comparison to C-mod data

Typical parameters for C-mod I-/H- plasmas at edge: $\rho_* \sim 0.006$,

$T_e \sim T_i \sim 200\text{eV}$, $\chi_i/\chi_\phi \sim 1$, $L_S \sim 0.6\text{m}$, $L_T \sim 0.01\text{m}$

▶ Dimensionless #:

▶ $\nu_* \sim 1.3 \gtrsim 1 \rightarrow$ trapped electron effects not of prime importance

▶ $c \equiv k_{\parallel}^2 v_{the}^2 / (\nu_{ei}\omega) \sim 30 \gg 1$ for $k_{\parallel} \sim 1/(qR)$, $k_{\perp}\rho_s \sim 0.2$

\rightarrow electrons are adiabatic

\Rightarrow model here (drift-ITG) is a reasonably good approximation

▶ Toroidal Flow Velocity $\langle V_{\parallel} \rangle / v_{thi}$ (Rice et al '10)

$$\frac{\langle V_{\parallel} \rangle}{v_{thi}} \cong \frac{\rho_*}{2} \frac{\chi_i}{\chi_\phi} \sqrt{\frac{T_i}{T_e}} \frac{L_S}{L_T} \sim 0.18$$

\Rightarrow Typical value in experiments: $\langle V_{\parallel} \rangle / v_{thi} \sim 0.1 - 0.3$

Conclusion

Intrinsic Rotation as a consequence of “plasma flow engine”

- ▶ **Entropy:** setting-up “engine” calculation

$$\int d\Gamma \left\{ \frac{\partial \langle \delta f^2 \rangle}{\partial t} \frac{1}{2 \langle f \rangle} + \frac{\partial \langle \tilde{V}_x \delta f^2 \rangle}{\partial x} \frac{1}{2 \langle f \rangle} + \frac{v_c \langle \delta f^2 \rangle}{\langle f \rangle} \right\} = \int d^3x \left(\frac{n \chi_i}{L_T^2} - \frac{n K \langle V_E' \rangle^2}{v_{thi}^2} \right)$$

\Rightarrow evolution via heat input, flow generation and spatial flux of entropy

- ▶ **Plasma Flow Engine:** conversion of heat to flow by residual stress

$$\frac{\langle V_{||} \rangle}{v_{thi}} = \underbrace{\frac{\rho_*}{2} \sqrt{\frac{T_i}{T_e}} \frac{\chi_i}{\chi_\phi} \frac{L_s}{|L_T|}}_{\nabla T \text{ driven, } \propto \nabla T / B_\theta} - \underbrace{\frac{\rho_*}{2} \sqrt{\frac{T_i}{T_e}} \frac{L_s}{2\Delta} \frac{1}{n} \int d^3v \int^x dx' \frac{1}{\chi_\phi} \left(-D_{spr} \frac{\partial \langle \delta f^2 \rangle}{\partial x} \frac{1}{2 \langle f \rangle} \right)}_{\delta f^2 \text{-flux driven} \rightarrow \text{jump in } \delta f^2 \text{ flux}} \Bigg|_{x'=-\Delta}^{x'+\Delta}$$

$\Rightarrow \langle V_{||} \rangle / v_{thi} \sim 0.18$ for C-mod parameters

- ▶ Future plan: Role of outflux of entropy, heat in intrinsic rotation drive?